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High Performance Size Exclusion Chromatography with Microparticulate Porous Silica Spheres. Influence of Flow Rate, Solute Mass Transfer and Polydispersity of Samples

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HIGH PERFORMANCE SIZE EXCLUSION CHROMATOGRAPHY
WITH MICROPARTICULATE POROUS SILICA SPHERES.
INFLUENCE OF FLOW RATE, SOLUTE MASS TRANSFER
AND POLYDISPERSITY OF SAMPLES

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ABSTRACT

The contributions to peak broadening in Size Exclusion Chromatography with microparticles of porous silica spheres having narrow size distributions have been determined by measuring the plate height dependence on flow rate for toluene and for polystyrene standards covering a wide range of molecular weights. From these contributions, the diffusion coefficients of the macromolecules in the pore matrix and the polydispersities of the samples could be evaluated. It is shown that for permeating polymers the band broadening is determined by the eddy diffusion in the mobile phase, by the slow mass transfer of the solute in the stationary phase and by the polydispersity of the standards. In properly packed columns the eddy diffusion term is of minor importance compared to the other effects, whereas the solute mass transfer, which is a velocity dependent

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process, can be minimized only at extremely low flow rates.

INTRODUCTION

Rigid inorganic packings are widely used in modern Size Exclusion Chromatography (SEC) because of their superior mechanical and thermal stability and their capability of withstanding the high pressures involved in high speed liquid chromatography. Since the efficiency of the SEC columns greatly increases by decreasing particle size (1), packing materials with particle average size of about $10\ \mu\text{m}$ or less are now produced: 25-30 cm long columns, packed with these microparticulate materials, show efficiencies several times higher than those of conventional SEC columns (2, 3).

Frequently, if not exclusively, the inorganic materials used in high performance SEC are porous silica gels. The determination of the molecular weights of polymers generally improves by decreasing the eluent flow rate: the situation is less critical when polymer samples of relatively broad molecular weight distribution are analyzed (accurate molecular weights have been obtained (4) with a flow rate of $0.5\ \text{cm}^3\ \text{min}^{-1}$), whereas with more narrowly distributed polymer samples one has to resort either to extremely slow flow rates (5), or to a suitable correction for peak spreading (4).

The flow rate dependence of the efficiency in SEC with short columns filled by silica microspheres of narrow size distribution and mean diameter $20\ \mu\text{m}$ and

8 μm was investigated by Dawkins and Yeadon (6, 7), who were successful in separating the different contributions which are operative in broadening the chromatographic peaks. Similar results were obtained with a different procedure by Knox and McLennan (8) who pointed out that in polymer size exclusion analysis with high performance columns the peak broadening is determined by the polymolecularity of the sample, which is the prevailing factor, and by a kinetic, flow rate dependent, contribution.

In the present paper the procedure suggested by Dawkins (6) to assess the importance of the different contributions to peak broadening and to determine the optimum working conditions is applied to packings of LiChrospher, a porous silica gel produced by E. Merck, Darmstadt, Germany, which has been found valuable in giving high resolutions in SEC, and which has already been the object of an investigation of one of us (4) on the use of it in molecular weight determinations by SEC. The present study has been performed on microparticles (about 10 μm) of different mean pore size, using polymer samples covering a wide range of molecular weights.

PEAK BROADENING IN SEC

In a properly arranged SEC system in which extracolumn effects, deriving from injection, capillary connections, detector, are minimized the peak broadening primarily depends on processes occurring in the column, and is a direct consequence of the slow rate of achie_

vement of solute equilibrium between the mobile and the stagnant phase. For macromolecules the time necessary to reach this equilibrium can be very long, so that local departures from equilibrium give raise to broadening and asymmetry of the peaks.

Peak broadening in chromatography is adequately expressed in term of the number N of plates of the column, and of the plate height H which can be defined as the peak variance per unit length of the column (9):

$$H = \sigma^2 / L \quad (1)$$

where σ is the peak standard deviation and L is the column length. For an experimental chromatogram the plate height is calculated from the relations:

$$H = L / N \quad (2)$$

$$N = 5.54 (V_e / w_{1/2})^2 \quad (3)$$

where V_e is the elution volume at the maximum of the peak and $w_{1/2}$ is the peak width at half height.

The theory of chromatography gives relationships in which the plate height is expressed in terms of sums of different contributions (10). From this general treatment the theory of peak dispersion in SEC was formulated by Giddings and Mallik (11) and applied to some experimental data (12), showing the reliability of the classical chromatographic approach to investigate even in the SEC case the peak broadening factors.

The dependence of plate height on the solute dispersion mechanism in SEC was subsequently investigated by Dawkins and Yeadon (5,6), who took into account the contribution from polydispersity in the elution of permeating polymers. In this case, the experimental value of H is given by

$$H = A + \frac{B}{u} + Cu + (\sigma_M^2 / L) \quad (4)$$

where u is the eluent flow rate, A, B and C are coefficients related to different diffusion processes of the solute molecules, and σ_M^2 / L is the contribution of the solute polydispersity (σ_M^2 is the peak variance depending on the molecular weight distribution). When standard polymer samples with low dispersity are eluted, assuming that their molecular weight distribution may be represented by a logarithmic normal one, the polydispersity term of eq. (4) takes the form:

$$\frac{\sigma_M^2}{L} = L \frac{\ln(M_w/M_n)}{D_2^2 V_e^2} \quad (5)$$

where D_2 is the slope of the SEC calibration curve, obtained by plotting $\ln M$ vs. V_e .

According to Giddings (10), the coefficients A, B and C of eq. (4) take the form:

$$A = 2 \lambda d_p \quad (6)$$

(where λ is a constant characteristic of the packing and d_p is the particle diameter),

$$B = 2 \gamma D_m \quad (7)$$

(where D_m is the diffusion coefficient of the solute in the mobile phase, corrected by the obstruction factor γ),

$$C = q R(1-R) \frac{d_p^2}{D_s} \quad (8)$$

(where q is a configuration factor depending on the particles' geometry, R is the retention ratio V_o/V_e between the interstitial volume of the column and the elution volume, and D_s is the solute diffusion coefficient in the pores).

By introducing eqs. (5), (6), (7) and (8) into eq. (4) one obtains:

$$H = 2 \lambda d_p + 2 \gamma \frac{D_m}{u} + q R(1-R) \frac{d_p^2}{D_s} u + L \frac{\ln(M_w/M_n)}{D_2^2 V_e^2} \quad (9)$$

which expresses the plate height as a sum of terms, the fourth of which depending upon the sample polydispersity, and the other three representing true chromatographic contributions: the first term (term A) comes from the eddy diffusion of the solute in the mobile phase, that is the fact that different solute molecules run

along different paths between the gel particles; the second term (term B) results from the longitudinal diffusion of the solute in the mobile phase; and the third (term C) comes from the mass transfer in the stationary phase associated with the slow diffusion of the solute in the packing pores.

By performing measurements with polymer samples differently excluded at different flow rates it is then possible, by applying eq. (9), to know how H varies and which factor is prevailing to change the efficiency of a given packing; the reliability of the packing procedure can also be checked together with the permeability characteristics of the porous material. Finally, by evaluating the last term of eq.(9), the polydispersity index M_w/M_n of the polymer standards can be calculated.

EXPERIMENTAL

LiChrospher packings with nominal particle size of 10 μ m were supplied by E. Merck (Darmstadt, Germany). Four different silica gels were used, SI 100 (batch no. YE604), SI 500 (batch no. YE91), SI 1000 (batch no. YE645) and SI 4000 (batch no. YE445), having different mean pore size. The microparticles, examined by optical microscopy, appeared to have a regular spherical shape. The densities of the different silica gels were determined with a picnometer.

The gels were dispersed in methanol, stirred in an ultrasonic bath, and the slurries were packed according

to the upward technique proposed by Bristow et al. (13) into stainless steel columns (length: 25 cm; internal diameter: 0.46 cm) at a pressure of about 10 MPa (1 MPa = 10 bar).

High performance SEC was executed with a dual-piston diaphragm pump (Orlita DMP-SK 15/3), and an ultraviolet detector (Zeiss, PM2 DLC, cell volume 8 μ l, 260 nm). An injection valve (Rheodyne 7010) with a 10 μ l loop was used to introduce the samples into the columns; all the connections between injector and column and between column and detector were made of short low dead-volume capillary tubing (0.025 cm i.d.).

The mobile phase was tetrahydrofuran (Carlo Erba, Milano, Italy) stored over KOH for 12 h, refluxed over CaH_2 and distilled. The samples injected were toluene (Carlo Erba) and polystyrene standards (ArRo Laboratories, Joliet, Illinois, and Polysciences, Warrington, Pennsylvania) dissolved in tetrahydrofuran at concentrations low enough to avoid concentration effects (14) on the elution volumes. For toluene and for PS standards up to about $M = 7 \cdot 10^5$ the sample concentration was 0.1% (w/v), whereas for the highest molecular weight standards it was 0.05% (w/v). The stream flow rate was detected in each analysis by measuring the time for collecting a given volume of the eluent in a burette connected with the output of the detector. With this system no short term flow rate variations were detected. The flow rates investigated varied from 0.15 to 2.5 $\text{cm}^3 \text{min}^{-1}$, corresponding to linear velocities ranging from about 0.03

to 0.6 cm sec^{-1} . Lower steady flow rates could not be obtained with the pumping system adopted.

The elution volumes of the injected samples were practically independent of the flow rate, except in a few cases at the highest velocities with the very high molecular weight standards. The reproducibility of the measurements was better than 1%. All the results for V_e and H are the average of at least three injections.

The characteristics of the packed columns were determined by direct calibration with the PS standards. For the column packed with SI 4000, however, the interstitial volume V_0 could not be determined with an excluded polymer because even a standard of molecular weight as high as $2.6 \cdot 10^7$ showed some permeation behaviour. Therefore the porosity of the SI 4000 gel was measured by titration, according to the method of Mottlau and Fischer (15). About 1 g of dry gel was weighed in a 50 cm^3 Erlenmeyer flask in which the titrating solvent (benzene) was slowly introduced by means of a plunger microburette; the gel was continuously stirred and the flask was connected to a benzene reservoir in order to eliminate solvent evaporation during the titration. The end point was taken when a small increment of liquid added to the gel, forming a very thin layer on the external surface of the particles, made them stick together to form a coherent caked mass. The specific porosity $V_{p,sp}$ of SI 4000 could then be calculated, and by multiplying it with the quantity of packing in the column, the pore volume V_p was obtained; from the latter and from the

elution volume of a totally permeating molecule, V_t , the interstitial volume $V_o = V_t - V_p$ was calculated. The titration method was checked, for our silica gels, by measuring the V_p of SI 500 and comparing it with the value obtained by SEC, with very good agreement (see Table 2).

RESULTS AND DISCUSSION

Characterization and calibration

From the particle size distributions as determined at intervals of 2 μm on the micrographs, the number average and weight average diameters reported in Table 1 were calculated according to the relations given by Dawkins et al. (16).

The results show small differences in the average particle size dimensions and narrow size distributions, particularly for SI 100 and SI 500. A narrow size distribution of particles is needed for high efficiency columns (16).

TABLE 1. Number Average and Weight Average Particle Diameters d_n and d_w and Polydispersity of Silica Particles.

<u>Silica</u>	<u>d_n (μm)</u>	<u>d_w (μm)</u>	<u>d_w/d_n</u>
SI 100	9.90	10.91	1.10
SI 500	8.20	9.30	1.13
SI 1000	8.14	9.67	1.19
SI 4000	7.66	9.10	1.19

The calibration curves, $\log M$ vs V_e , of the single columns packed with the different silica gels were determined at an eluent flow rate of about $0.5 \text{ cm}^3 \text{ min}^{-1}$ and are shown in Fig. 1. Toluene was the totally permeating solute. It can be seen from the figure that SI 500 and SI 1000 gels have quite similar pore dimensions, and that the SI 4000 column shows a lower pore volume

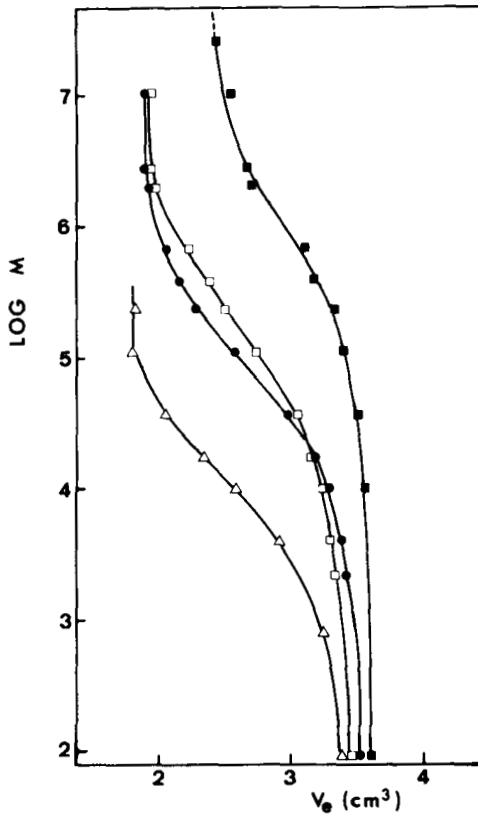


FIGURE 1. SEC calibration curves for polystyrene standards; Δ , SI 100 silica; \bullet , SI 500 silica; \square , SI 1000 silica; \blacksquare , SI 4000 silica.

than the others. From the calibration data the quantities of interest in SEC can be extracted: V_0 and V_t from the elution volumes of excluded and totally permeating solutes respectively, V_p from the difference $V_t - V_0$, and V_s , the volume of solid silica in the column, from the relation $V_s = V_{col} - (V_0 + V_p)$, where the volume of the empty column, V_{col} , was 4.155 cm^3 . With the V_s values and the measured densities of the solid part of the microspheres the quantity of silica in the different packed columns was calculated. (For the SI 4000 column V_p was obtained from the specific pore volume determined by titration).

In Table 2 are reported all the characteristics data of the packed columns. The SI 4000 column has a significantly lower quantity of gel than the other columns and this fact brings about the low value of V_p , together with the high value of V_0 . It appears that the smaller

TABLE 2. Density Values of the Silica Particles and Characteristics of the Packed Columns.

Silica	Density g cm^{-3}	Grams of Packing	V_0	V_p cm^3	V_t	V_s
SI 100	2.03	1.54	1.79	1.60	3.39	0.76
SI 500	2.11	1.33	1.89	1.64 1.65*	3.53	0.63
SI 1000	2.27	1.57	1.92	1.55	3.47	0.69
SI 4000	2.22	1.24	2.36*	1.24*	3.60	0.56

* by pore titration

dimensions of these particles make it more difficult to obtain a superior quality packing. For all the columns the efficiency determined according to eq. (3) from the toluene peak gave values higher than 20000 plates m^{-1} .

Dependence of H on flow rate

In Fig. 2 are reported the dependences of H on eluent flow rate for different solutes eluted in the LiChrospher SI 100 column. Toluene is a totally permeating molecule, PS 10000 and PS 37000 are partially permeating PS standards, and PS 111000 and PS 233000 are two excluded PS standards.

It can be seen that for toluene there is a very low decrease of the H values with decreasing flow rate,

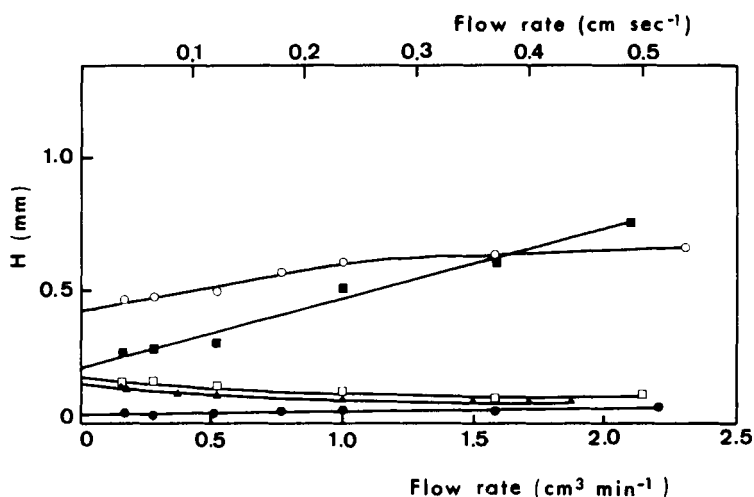


FIGURE 2. Dependence of plate height on flow rate for SI 100 silica: ●, toluene; ○, PS 10000; ■, PS 37000; □, PS 111000; ▲, PS 233000.

without any tendency of H to increase at the lowest flow rates investigated. In terms of eq. (9) this means that the contribution of the longitudinal diffusion in the mobile phase (term B) can be neglected; the polydispersity term is non operative for toluene, and the small dependence of H on flow rate indicates that the term for solute mass transfer in the stationary phase (term C) is not very important for molecules having high values of D_s . Therefore the main contribution to H for a small molecule comes from the eddy diffusion in the mobile phase (term A). Also the excluded polymers show a low variation of H with flow rate. For these solutes term C vanishes ($1-R = 0$), and the polydispersity term is not to be taken into account because there is no permeation into the pores. The slight increase of H at the lowest flow rates cannot be attributed to term B because, for the very low values of D_m of these molecules the longitudinal diffusion is negligible at the flow rates employed; the effect shown in Fig. 2 is similar to that observed by Knox and McLennan (8) on solute dispersion of excluded polymers, and attributed to a partial penetration of the macromolecular coils into the largest pores of the packing, which becomes evident at low flow rates. Such an interpretation is in agreement with the higher values of H for PS 111000 than for PS 233000, and with the finding of highly tailed chromatographic peaks at the low flow rates.

For the two permeating polymers term C and the fourth term of eq. (9) are important in determining the

values of H and their dependence on flow rate. The increase of H with increasing flow rates depends on the ratio $R(1 - R)/D_s$ of term C , whereas the vertical displacement of the curves with respect to the H values of toluene results from the polydispersity of the samples. The flattening experimentally found in the curve of PS 10000 at $u > 1 \text{ cm}^3 \text{ min}^{-1}$ is not accounted by eq. (9); a decrease of the slope of these curves with increasing eluent velocities was reported by van Kreveland and van den Hoed (17) to occur at linear velocities higher than ours: such an effect increased with increasing molecular weight of the solute. It has been suggested that at high flow rates flow into the pores could facilitate the mass transfer between the mobile and the stationary phase, but no rigorous interpretation of this phenomenon is available; a better description of mass transfer effects within the pores should be supported by a detailed knowledge of the pore structure.

The curves showing the dependence of H on eluent flow rates for the SI 500, SI 1000 and SI 4000 columns are reported in Figs. 3-5. In these columns excluded polymers, when available, were not analysed at different flow rates because the very high molecular weight standards gave broad and distorted peaks which were difficult to measure. For the other solutes the behaviour was analogous to that of SI 100. The elution of toluene at the different flow rates gave practically no variation of H . With SI 4000 the peaks of toluene were somewhat less symmetrical than for the other columns,

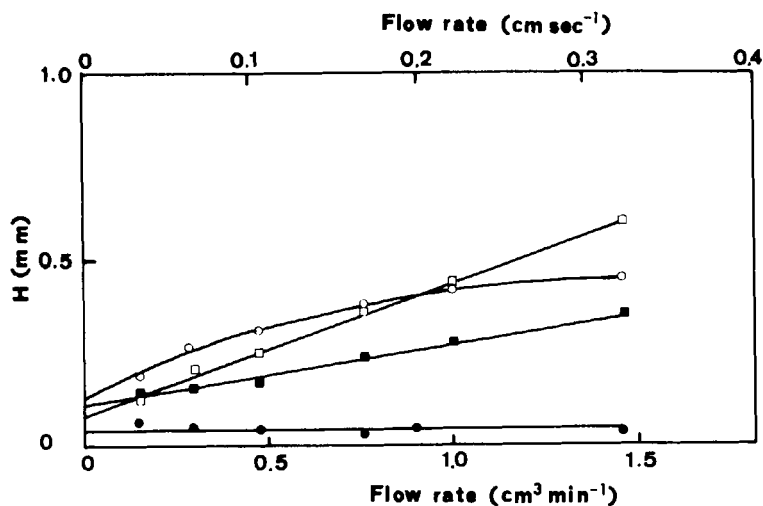


FIGURE 3. Dependence of plate height on flow rate for SI 500 silica: ●, toluene; ■, PS 37000; □, PS 111000; ○, PS 390000.

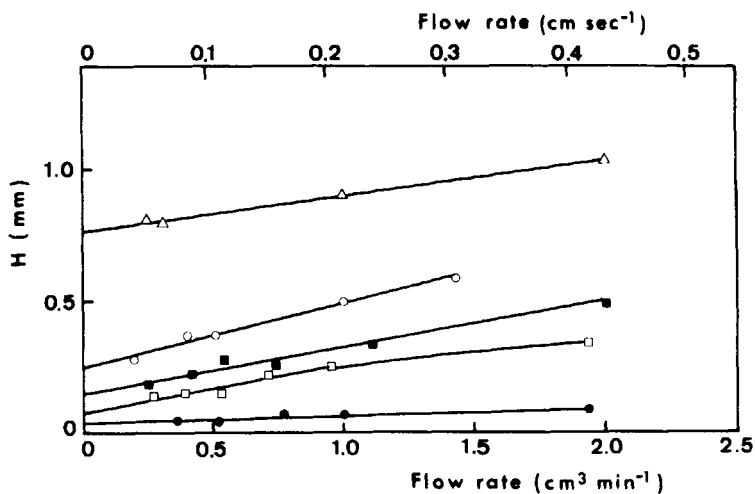


FIGURE 4. Dependence of plate height on flow rate for SI 1000 silica: ●, toluene; □, PS 37000; ■, PS 111000; ○, PS 390000; △, PS 2050000.

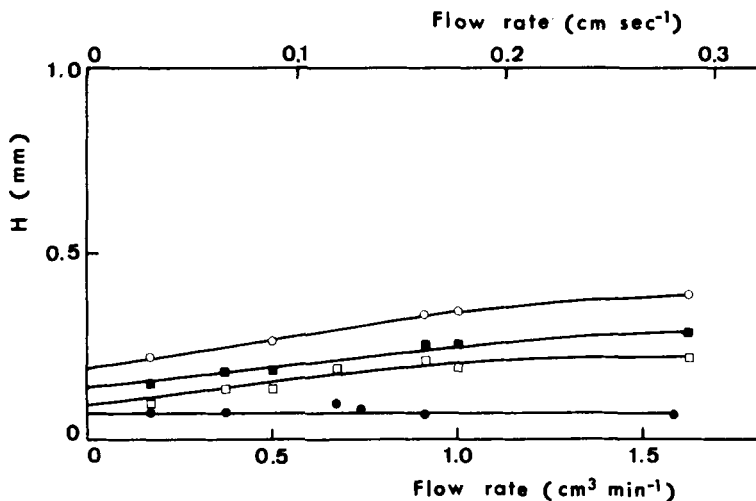


FIGURE 5. Dependence of plate height on flow rate for SI 4000 silica: ●, toluene; □, PS 111000; ■, PS 390000; ○, PS 670000.

and this might be attributed to the less homogeneous packing bed obtained with this gel. The permeating polymers show higher H values than for toluene, increasing with flow rate because of the mass transfer of the solute in the stationary phase. The expected dependence of H on flow rate is also evident in the SI 1000 column for the elution of PS 2050000, which permeates only a small portion of pores (see Fig. 1). The strong vertical displacement of the curve for this standard with respect to the other curves clearly indicates that the polydispersity of the polymer is not very low.

Diffusion coefficients of polystyrenes in the pores

From the slope of the linear part of the H vs linear velocity curves of Figs. 2-5 the term of solute disper_

sion resulting from mass transfer of the permeating samples in the stationary phase can be obtained. When the packing material is constituted by a collection of spherical particles with a size distribution, the value of the configuration factor q is $1/30$ (12), and the correct mean particle diameter \bar{d}_p must be introduced in term C of eq. (9). The \bar{d}_p which is to be applied is the volume-weighted average value (12), which for particles of the same material is equal to the weight average diameter d_w . Therefore term C of eq. (9) becomes

$$\frac{R(1 - R) d_w^2}{30 D_s}$$

and the values of the diffusion coefficients D_s of polystyrenes in the pore structure are easily calculated from the experimental slopes of Figs. 2-5. The D_s values can be compared with the diffusion coefficients at infinite dilution, D_m , of the polymers in free solution, and the ratio D_s/D_m , representing the hindrance to the molecule diffusion in the pores, is obtained. The values evaluated for the four silica gels investigated are reported in Table 3. The D_m values for the PS standards were calculated according to the relationship

$$D_m (\text{cm}^2 \text{sec}^{-1}) = 3.45 \cdot 10^{-4} M_w^{-0.564}$$

valid in tetrahydrofuran at 24 °C for PS samples in the molecular weight range up to about $2 \cdot 10^6$ (18).

From the data of Table 3 one can see that for the same molecule eluting in different silica gels the D_s value increases with increasing mean pore size, as it is to be expected, but all the D_s values are much lower than the D_m values, indicating that the diffusion of the macromolecules in the pores is severely hindered. The results obtained in this study are completely comparable with those reported in the Literature for dif_

TABLE 3. Diffusion Coefficients of Polystyrene Standards Evaluated on LiChrospher Silicas with Mean Particle Dimensions d_w .

Standard	Column	d_w (μm)	$D_s \cdot 10^8$ ($\text{cm}^2 \text{sec}^{-1}$)	$D_m \cdot 10^8$ ($\text{cm}^2 \text{sec}^{-1}$)	D_s/D_m
PS 10000	SI 100	10.91	11.23	190.00	0.06
PS 37000			4.24	92.00	0.05
PS 37000	SI 500	9.30	8.84	92.00	0.10
PS 111000			3.52	49.70	0.07
PS 390000			1.81	24.00	0.07
PS 37000	SI 1000	9.67	8.89	92.00	0.10
PS 111000			8.46	49.70	0.17
PS 2050000			2.51	9.70	0.26
PS 111000			12.30	49.70	0.25
PS 390000	SI 4000	9.10	9.97	24.00	0.41
PS 670000			5.84	18.00	0.32

ferent packings: Giddings et al. (12) reported a value $D_s/D_m = 0.17$ for low molecular weight polymers in porous glass ($\bar{d}_p = 59 \mu\text{m}$); Dawkins and Yeadon (19, 7) have determined on silica microspheres D_s/D_m values in the range 0.11-0.19 ($\bar{d}_p \approx 20 \mu\text{m}$) and 0.08 - 0.15 ($\bar{d}_p \approx 8 \mu\text{m}$), and similar results were obtained by Knox and McLennan (8), who reported D_s/D_m values in the range 0.06 - 0.17 ($\bar{d}_p \approx 7.5 \mu\text{m}$), and by van Kreveld and van den Hoed (17) who calculated on Porasil silica ($\bar{d}_p = 75 - 125 \mu\text{m}$) values decreasing from 0.312 to 0.119 by increasing the molecular weights of PS standards from 20000 to 160000. The D_s/D_m values of Table 3 vary from 0.05 to 0.41 in the different column systems, and no definite trend is shown by changing the molecular weights in the same silica gel. It can be suggested that the restriction ratio D_s/D_m varies not only with the packing porosity and with the molecular weight of the eluted samples but also with differences in the internal pore structure or in the pore size distribution. Therefore to interpret D_s/D_m variations a more detailed knowledge of the real pore structures would be needed. In any case, it can be concluded that, independently of the particle size dimensions, the transfer of solute molecules from mobile to stationary phase in the porous particles used in SEC is very slow.

Polydispersities of the polystyrene standards

From the linear part of the curves of permeating polymers in Figs. 2-5 it is possible to extrapolate the intercept value H_{PS}^{int} . By assuming that this value appro_

ximates the plate height H_{PS}^* at very low eluent flow rates, but where the term B of eq. (9) would not be large and considering that at these low flow rates the contribution to H of term C is negligible with respect to the eddy diffusion term, one obtains from eq. (9):

$$H_{PS}^{int} \approx H_{PS}^* = 2 \lambda d_p + (L \ln \frac{M_w}{M_n} / D_2^2 V_e^2) \quad (10)$$

Therefore the plate height H_{PS}^{int} of eq. (10) is the sum of an eddy diffusion term and a term deriving from the sample polydispersity. The results shown above indicate that the eddy diffusion term can be well approximated by the plate height value of toluene H_t^{int} calculated at $u = 0$; this value can be substituted for $2 \lambda d_p$, and the second term on the right hand side of eq. (10) can be evaluated. From this term the values M_w/M_n of the dispersities of the permeating polymers have been calculated in the different column systems and the results are shown in Table 4.

The values of M_w/M_n calculated from plate height data are quite reasonable, according to the characteristics of these "monodisperse" standards; the relatively high dispersity found for PS 2050000 is also in agreement with the fractionation data given by the supplier, and with the general higher dispersity of these high molecular weight standards. The results of Table 4 compare well with those obtained by other Authors on different PS standards, prepared as well by living anionic polymerization (6 - 8). However, having investiga_

TABLE 4. Polydispersity of Polystyrene Standards Calculated from Eq. (10).

Polymer	Column	H_{PS}^{int} (mm)	H_t^{int} (mm)	M_w/M_n
PS 10000	SI 100	0.430	0.030	1.073
PS 37000	SI 100	0.210	0.030	1.020
	SI 500	0.110	0.040	1.017
	SI 1000	0.080	0.040	1.019
PS 111000	SI 500	0.088	0.040	1.009
	SI 1000	0.150	0.040	1.042
	SI 4000	0.100	0.070	1.040
PS 390000	SI 500	0.130	0.040	1.043
	SI 4000	0.140	0.070	1.038
PS 670000	SI 4000	0.190	0.070	1.062
PS 2050000	SI 1000	0.770	0.040	1.160

ted the performance of silica particles with different pore size distributions, the present evaluation of the polydispersities of PS standards covers a broader molecular weight range. The agreement obtained in the results for the same polymer in different columns is relevant and further supports the applicability of this chromatographic procedure for evaluating band broadening

in high performance SEC, in spite of the approximations involved in the calculations.

CONCLUSIONS

The application of classical chromatographic equations, adequately modified, to high performance SEC has proved to be a useful tool in the investigation of the relative importance of the different processes which determine the band broadening, and in the evaluation of the permeability characteristics of the porous packings. In high performance SEC the main dispersion process occurring in the mobile phase is the eddy diffusion of solute molecules. Its contribution to plate height is minimized by using packings made of small spherical particles with narrow size distribution. For high molecular weight polymers, permeating the porous material, the band broadening is also determined, in addition to the size fractionation due to the polydispersity of the solute, by the mass transfer of the polymer molecules in the stationary phase, which is a slow and velocity dependent process. It follows that also at even lower linear velocities the plate height contribution from this term is by no means negligible, at least for polymers having low dispersities. On the other hand, for polymers broadly distributed the contribution from polydispersity will quickly predominate over the dispersion phenomena occurring in the mobile phase, and with the values of the mass transfer coefficients generally found in the SEC packings, it should be possible to obtain re_

liable molecular weight distribution data working at a_ about 0.1 cm sec^{-1} without broadening corrections.

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